



# Status of SC Undulator Studies in the UK

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**ASTeC**

on behalf of the Daresbury and Rutherford  
Appleton Laboratories SCU Team

# Contents

- Introduction
- SC Helical Undulators
- SC Planar Undulators
- Measurement of material properties
- Summary



# Setting the Scene

- **RAL** has a long and distinguished history in the field of SC magnets and more recently with closed loop cryogenic systems
  - SC magnets particularly for particle physics applications
  - Cryocoolers primarily for space applications
- **Daresbury** has a similar position in the field of light sources and undulators
- **Since 2004 the two groups have worked together on SCUs**
- Recently **Diamond** has also joined the team



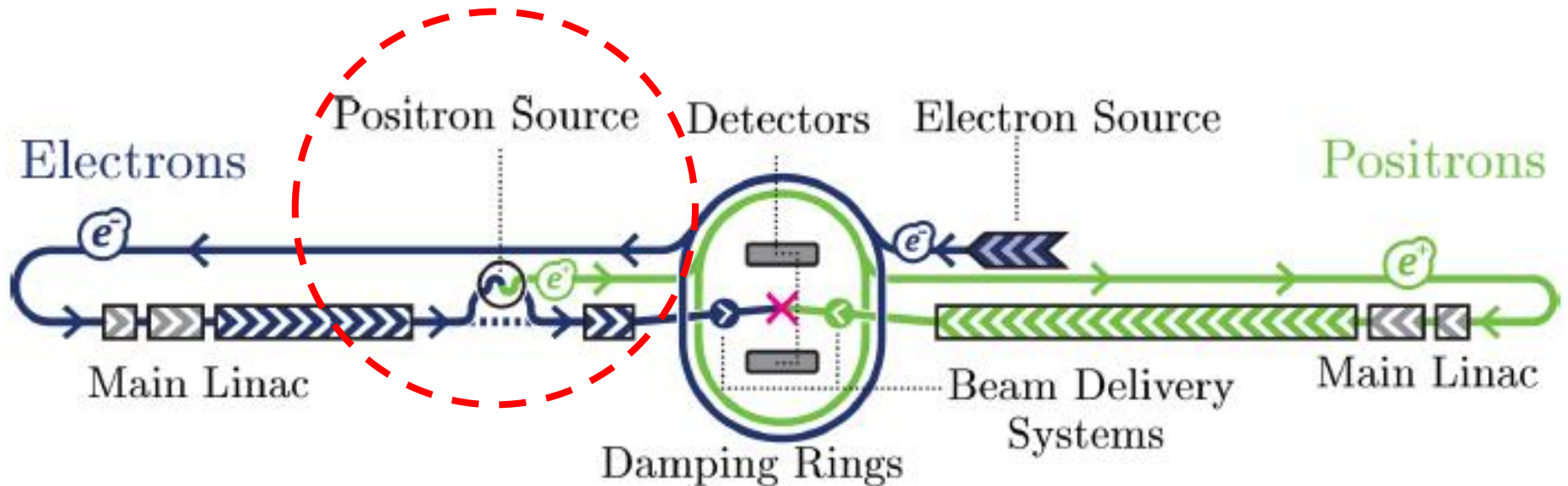
# Helical SCU Motivation

- The International Linear Collider requires unprecedented numbers of positrons when compared with present day sources
- If the positrons can be **polarised** then the physics reach of the collider can be enhanced
- **ILC Baseline** – Synchrotron radiation from an undulator
  - Very high energy electrons
  - Short period undulator
  - Lots of Periods for high intensity
  - Helical undulator → circularly polarised photons

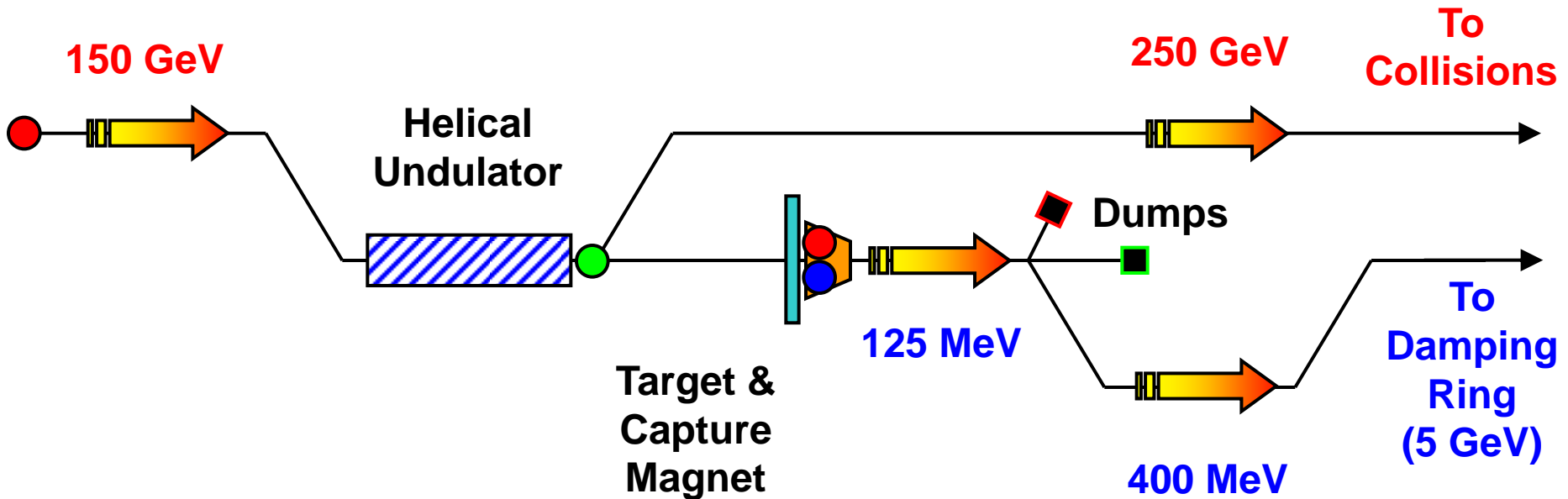


# The ILC

- The ILC is a proposed **electron-positron collider**
- Both beams have maximum energy **250 GeV**
- Total length of facility **~35 km**



# Positron Source Layout (RDR)



- **10MeV+ photon beam** generated in helical undulator by **150 GeV electrons**
- Photon beam travels ~400 m beyond undulator and then generates  $e^+e^-$  pairs in **titanium alloy target**
- Positrons captured and accelerated to 125 MeV
- Any electrons and remaining photons are then separated and dumped
- Positrons further accelerated to **400 MeV** and transported for ~5km
- Accelerated to 5 GeV and **injected into Damping Ring**

# The Undulator

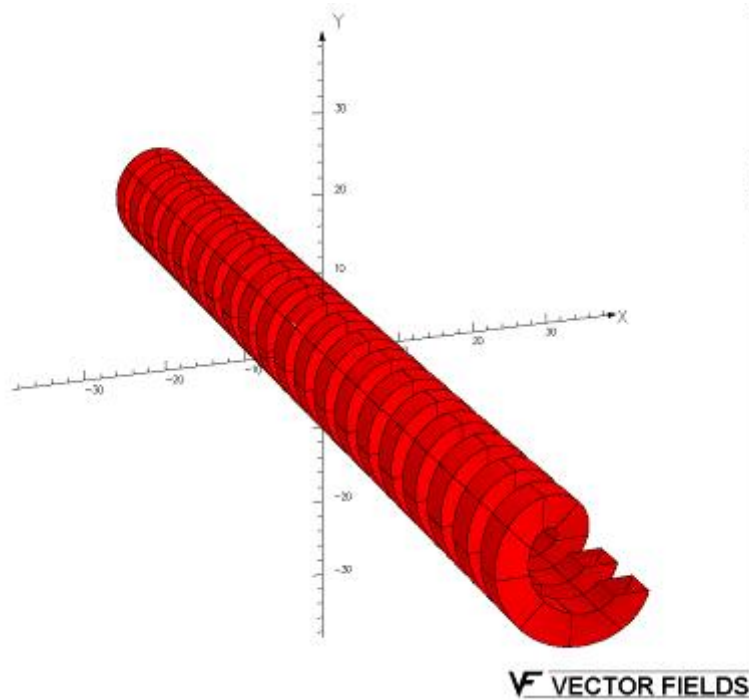
- To generate the photons with a high enough energy (>10MeV) need to use **short period, high field**, undulator
- For sufficient positrons undulator must be **~200m**
- Short period, high field, only possible with **narrow aperture**:
  - Resistive wall effects
  - Vessel surface roughness effects
  - Synchrotron radiation power problems
  - Generating a vacuum with difficult aspect ratio
  - Mechanical tolerances
  - Manufacturing issues
- **Superconducting** technology solution chosen after 'competition' with permanent magnet



# Magnet Design

- **Bifilar Helix with iron poles**
- **NbTi wire**
- **Non-magnetic vacuum vessel**

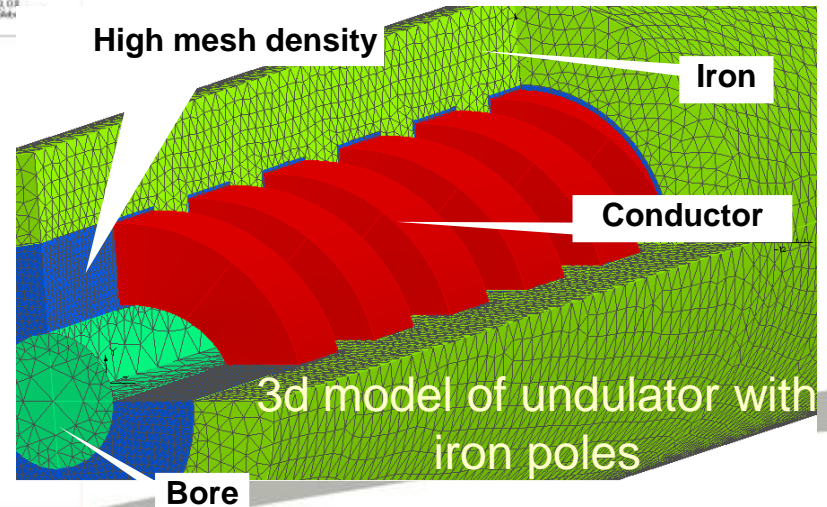
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| UNITS             |                  |
|-------------------|------------------|
| Length            | m                |
| Magn Flux Density | T                |
| Magn Field        | A/m              |
| Magn Vector Pot   | V                |
| Magn Vector Pot   | V/m              |
| Vec Flux Density  | C/m <sup>2</sup> |
| Vec Field         | V/m              |
| Conductivity      | S/m              |
| Current Density   | A/m <sup>2</sup> |
| Power             | W                |
| Force             | N                |
| Energy            | J                |

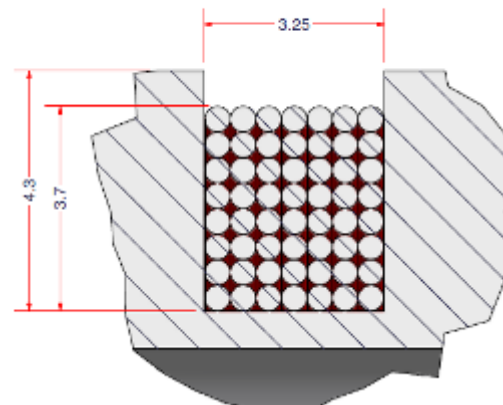
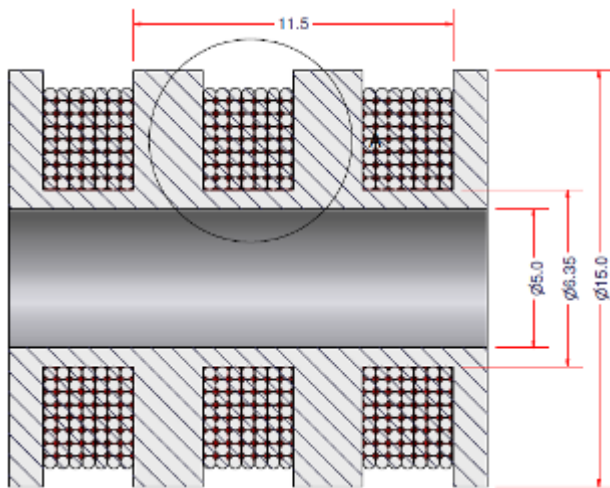
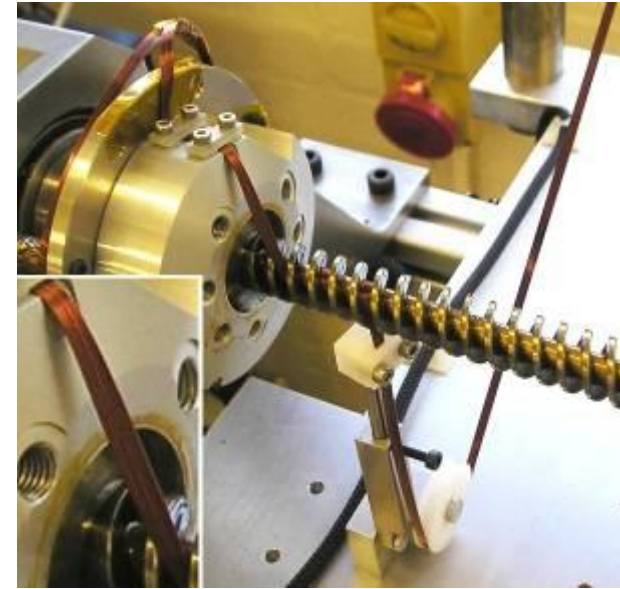
| FEMM DATA         |            |
|-------------------|------------|
| 3D conductor      |            |
| Local Coordinates |            |
| Origin            | 0, 0, 0, 0 |
| Local X12         | = Global   |



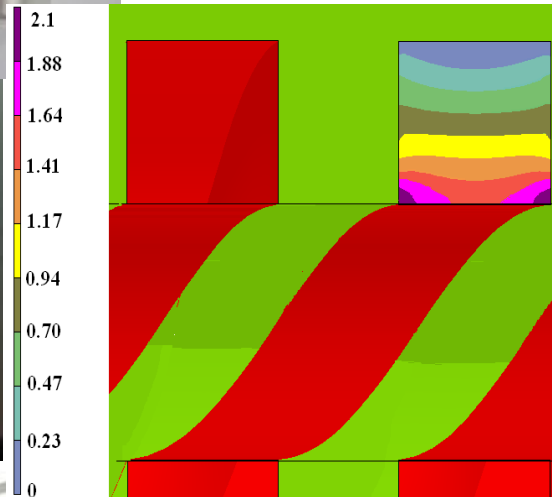


# NbTi Winding

- Wound with **7 wire ribbon**, 8 layers
- **0.4 mm NbTi wire**, with **25  $\mu$ m enamel** (0.45 mm when insulated)
- **3.25 mm wide winding** for **11.5 mm period**
- **Packing Factor of 62%**



# NbTi Prototypes

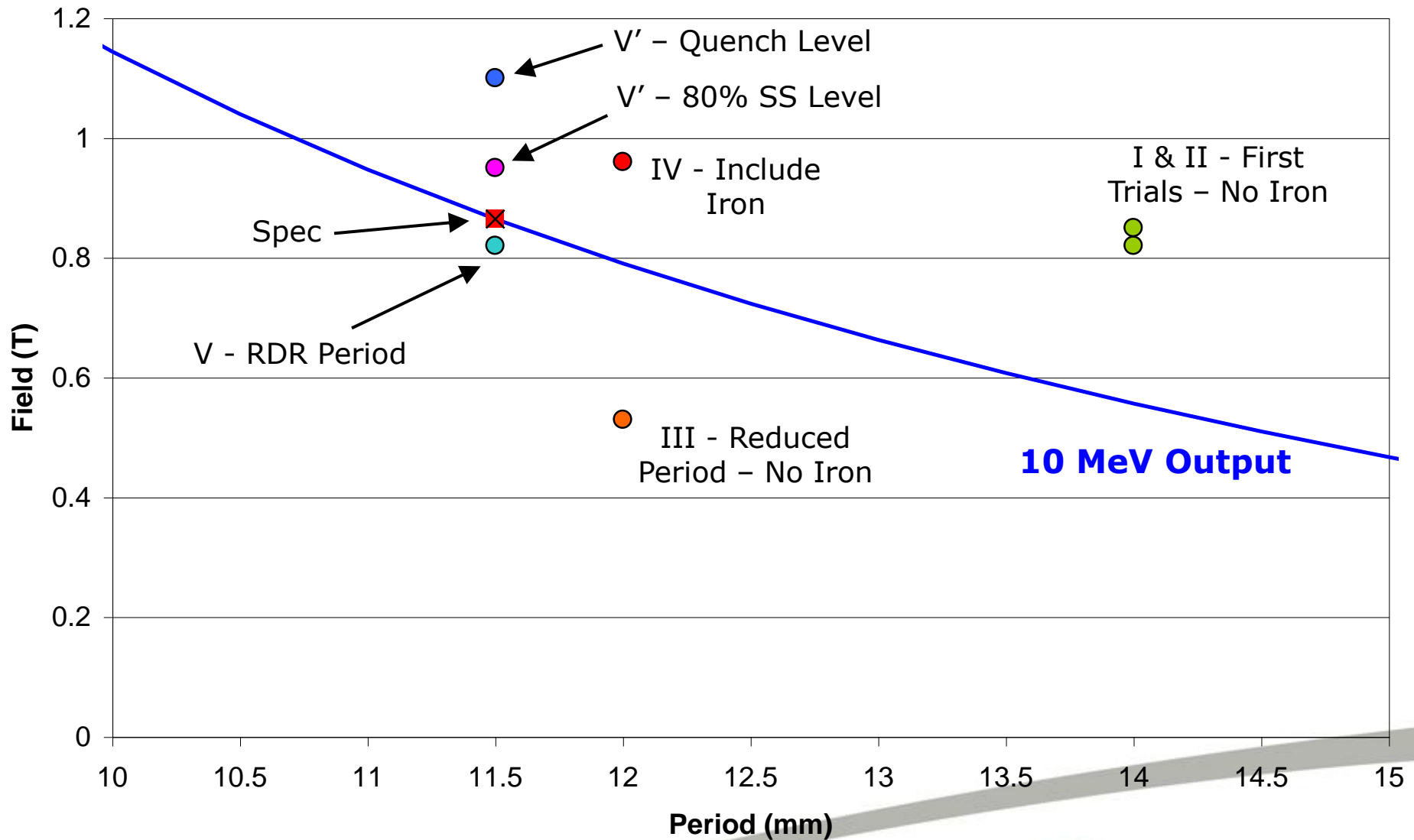


# Prototypes Summary

| Parameter       | Prototype 1                | Prototype 2                | Prototype 3                | Prototype 4                | Prototype 5                | Prototype 5'               |
|-----------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| Prototype goal  | Winding Technique          | Mechanical tolerances      | Reduced period             | Check effect of iron       | Increased period           | improved impregnation      |
| Length          | 300 mm                     | 300 mm                     | 300 mm                     | 300 mm                     | 500 mm                     | 500 mm                     |
| Former material | Aluminium                  | Aluminium                  | Aluminium                  | Iron                       | Iron                       | Iron                       |
| Bore tube       | Integral                   | integral                   | integral                   | integral                   | copper                     | copper                     |
| Winding period  | 14 mm                      | 14 mm                      | 12 mm                      | 12 mm                      | 11.5 mm                    | 11.5 mm                    |
| Winding bore    | 6 mm                       | 6 mm                       | 6 mm                       | 6 mm                       | 6.35 mm                    | 6.35 mm                    |
| Magnet bore     | 4 mm                       | 4 mm                       | 4 mm                       | 4.5 mm                     | 5.23 mm                    | 5.23 mm                    |
| SC wire         | Cu:SC<br>1.35:1            | Cu:SC<br>1.35:1            | Cu:SC<br>1.35:1            | Cu:SC<br>1.35:1            | Cu:SC<br>0.9:1             | Cu:SC<br>0.9:1             |
| Winding         | 8-wire ribbon,<br>8 layers | 9-wire ribbon,<br>8 layers | 7-wire ribbon,<br>8 layers | 7-wire ribbon,<br>8 layers | 7-wire ribbon,<br>8 layers | 7-wire ribbon,<br>8 layers |



# Prototypes Summary



# Full Undulator Parameters

| Undulator Parameters                            | Symbol     | Value   | Units |
|---|------------|---------|-------|
| Undulator period                                | $\lambda$  | 1.15    | cm    |
| Undulator strength                              | K          | 0.92    |       |
| Undulator type                                  |            | helical |       |
| Active undulator length                         | $L_u$      | 147     | m     |
| Field on axis                                   | B          | 0.86    | T     |
| Beam aperture                                   |            | 5.85    | mm    |
| Photon energy (1 <sup>st</sup> harmonic cutoff) | $E_{c10}$  | 10.06   | MeV   |
| Photon beam power                               | $P_\gamma$ | 131     | kW    |

Undulator to be made of 4m long modules



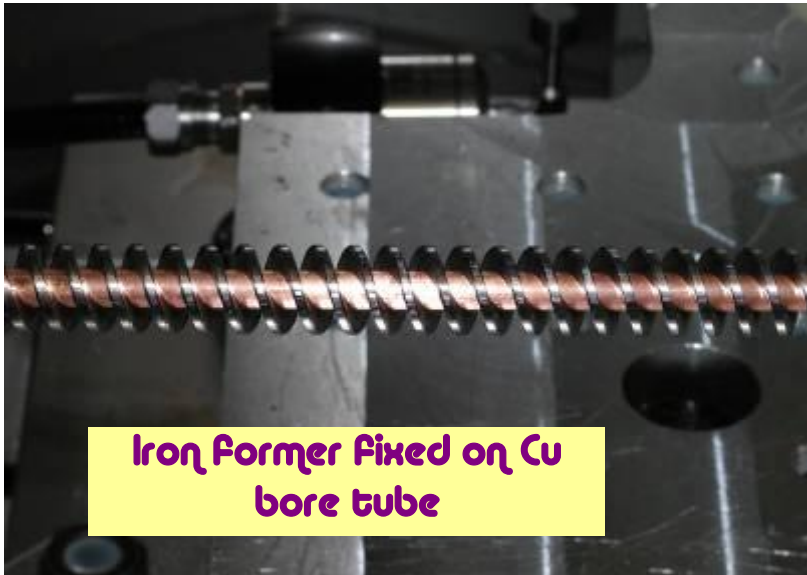
# 4th Prototype manufacture



4 axis machining

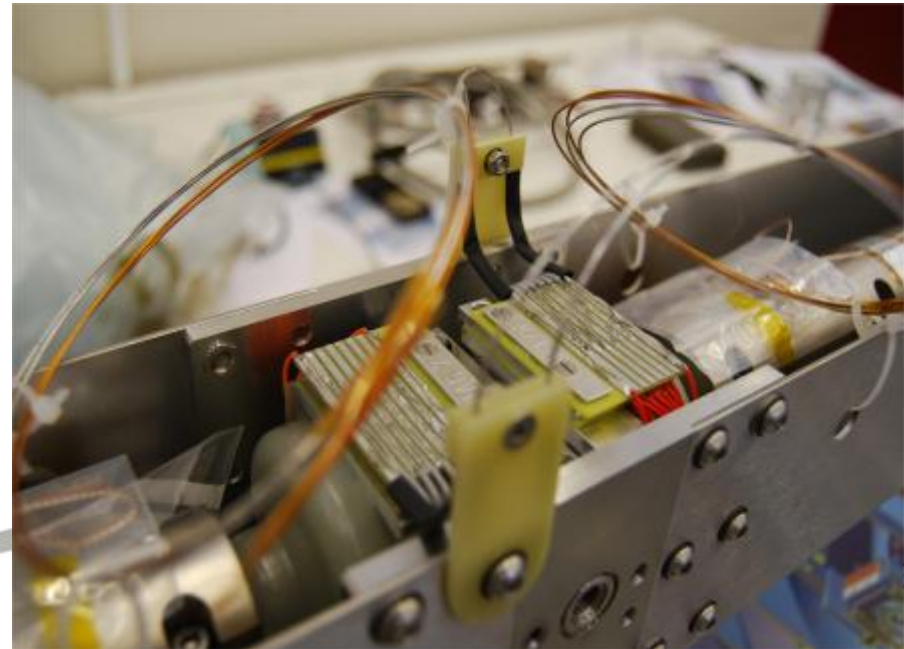
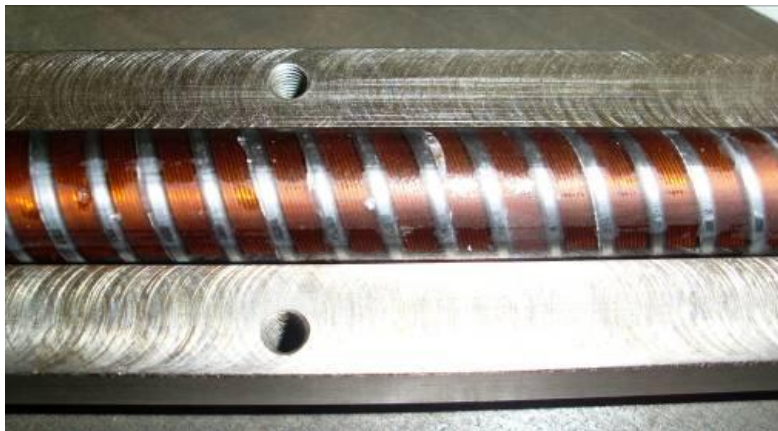
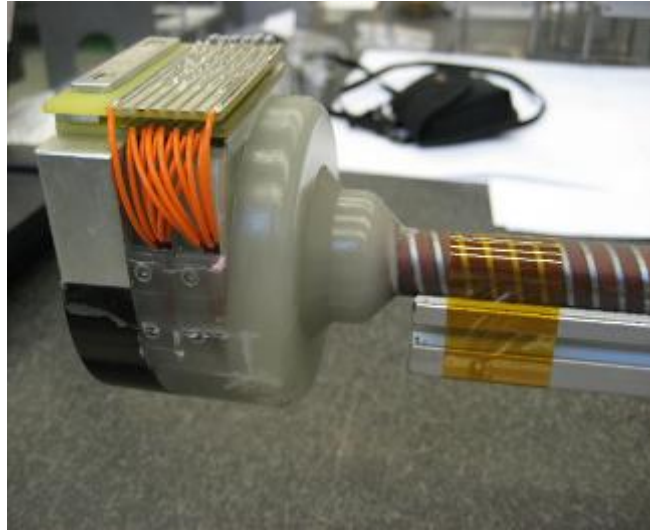


Coil winding

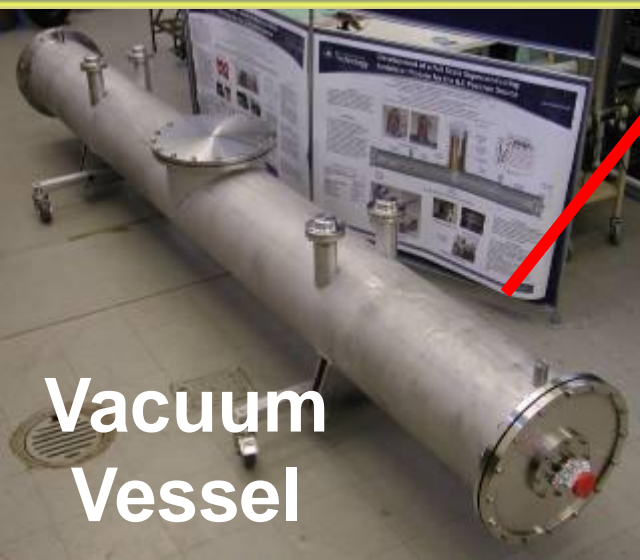
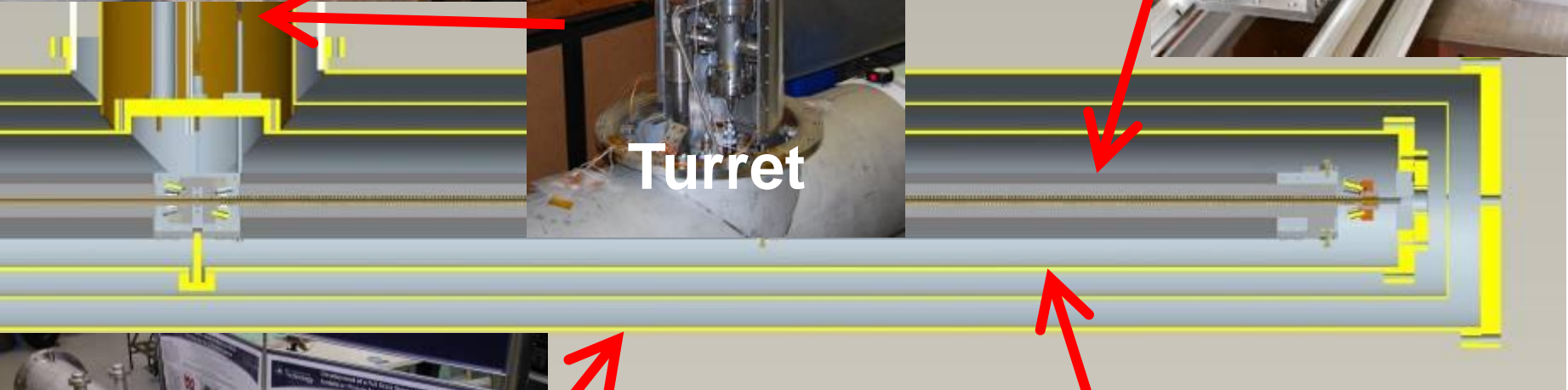


Iron Former Fixed on Cu  
bore tube

# 4m Prototype manufacture



# 4m Cryomodule Fabrication





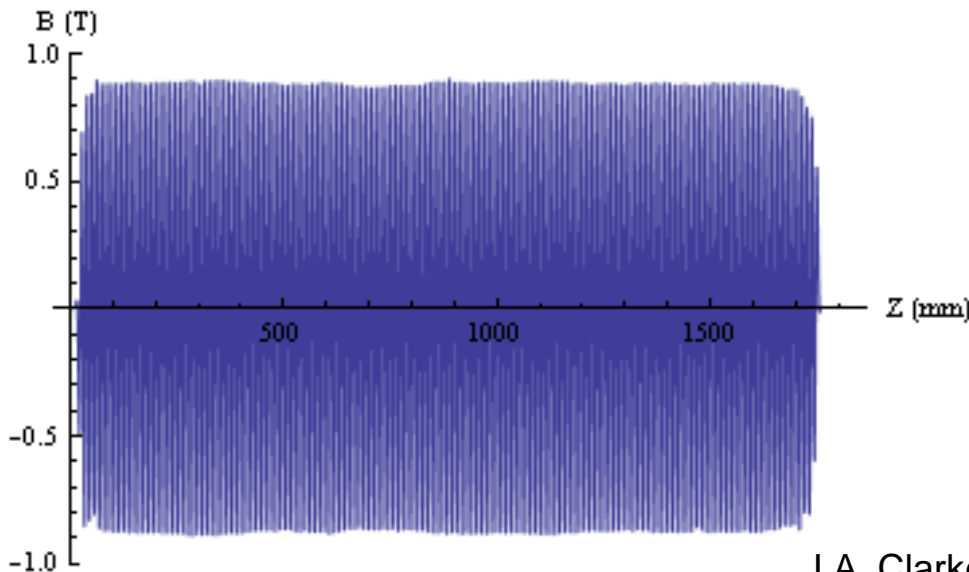
# Cryomodule

- A 4m module containing 2 x 1.75m helical undulators (11.5 mm period) has been constructed
- Closed loop cryo system with cryocooler

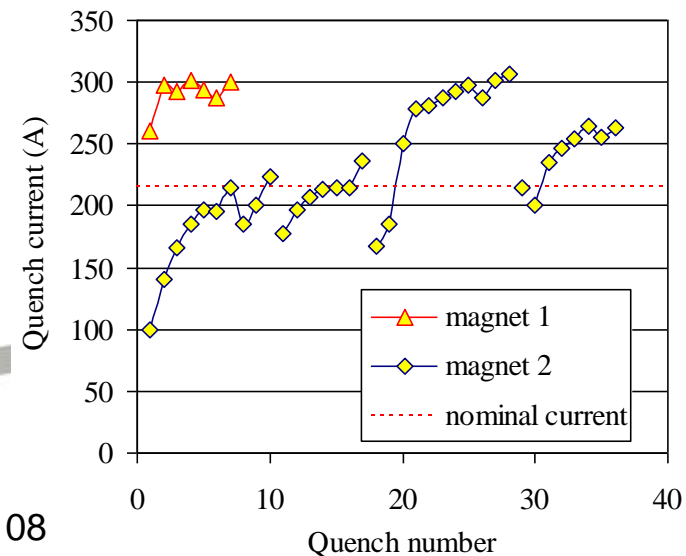


# Vertical Tests

- The quench test results show different behaviour between the two identical magnets
- Both do actually reach the same final quench current which agreed well with expectations
- **300A = 1.15T (spec is 0.86T, 215A)**

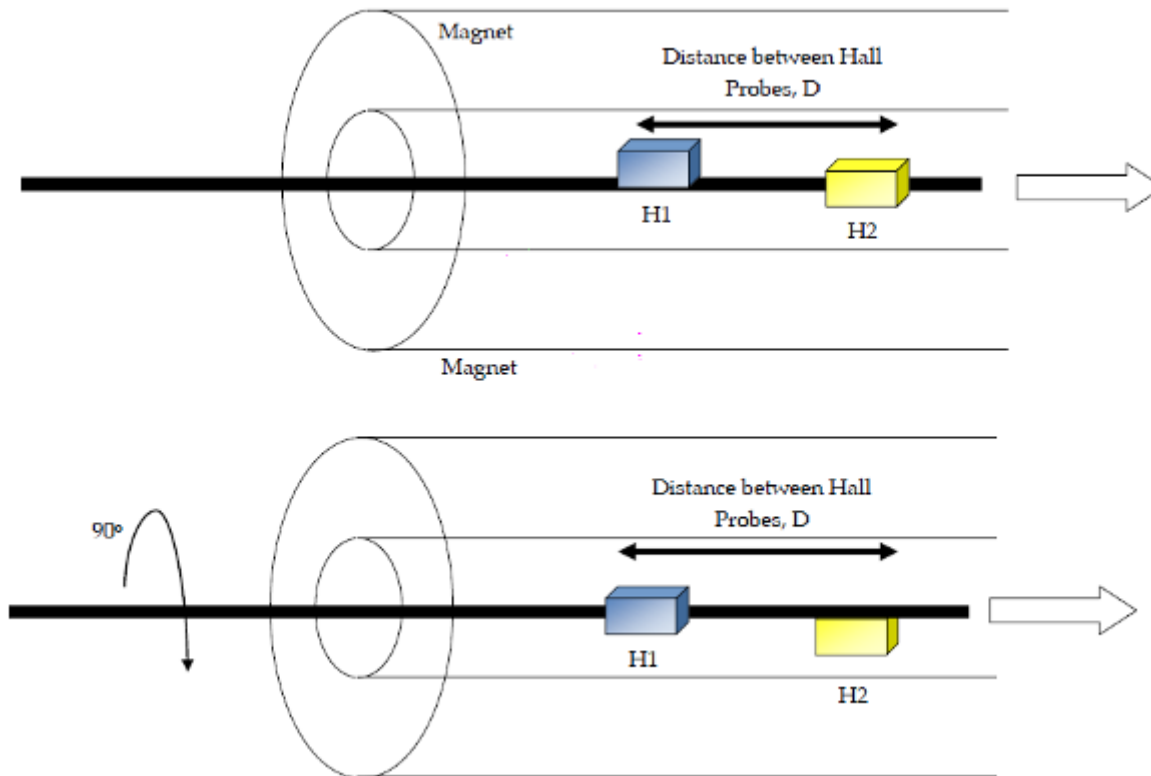


J.A. Clarke et al, EPAC 08



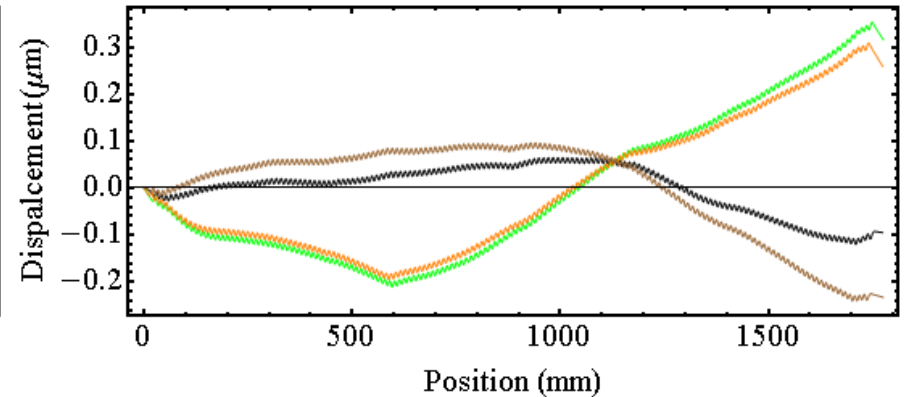
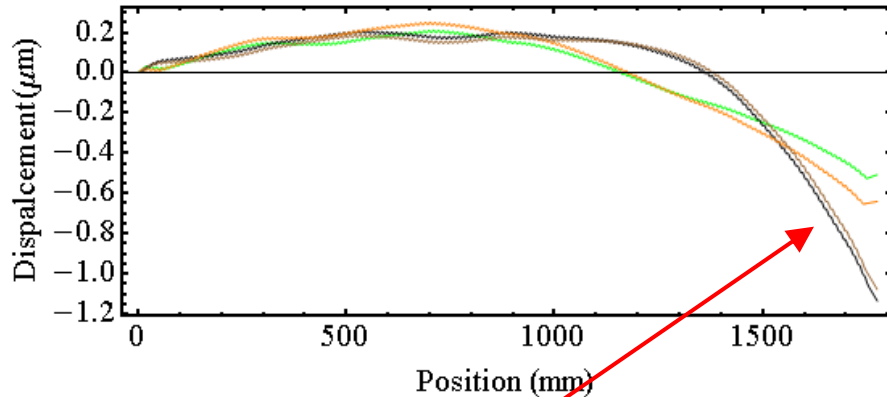
# Measurement Details

- 2 orthogonal Hall probes x 4 orientations = 8 measurements per magnet



# Trajectories

- Combine 180 deg results to cancel planar Hall effect
- H1 and H2 trajectories very similar
- Magnet 1 left, Magnet 2 right



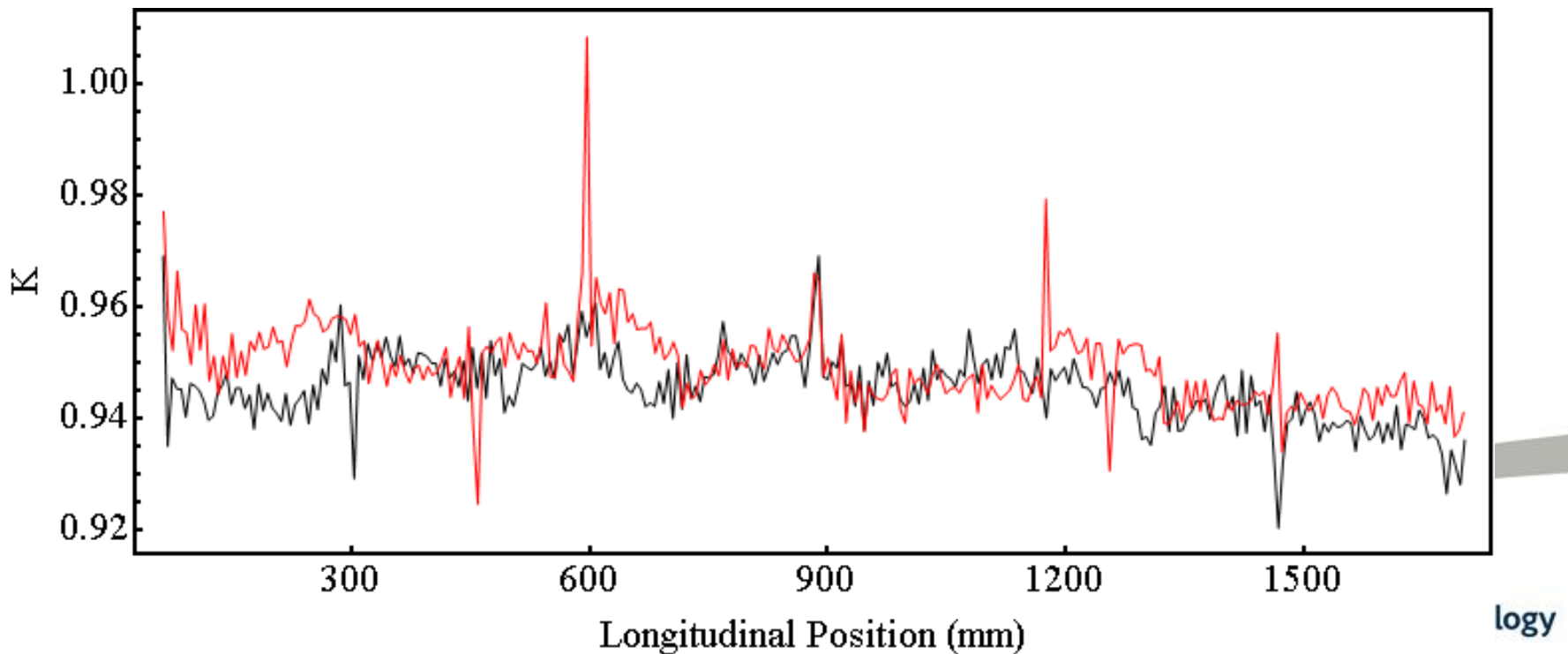
“Dipole field” – very hard to explain!

It is in all the raw data but only in one field component.

Unable to generate in any magnet model including errors

# K along length

- M1 black, M2 red
- Spikes are due to “Indexing points” from former manufacture
- Tighter control on former machining would remove these



# Phase Error

- X (red) and Y (blue) components of the field
- Phase generally very good except dipole part of M1!
- Magnet 1

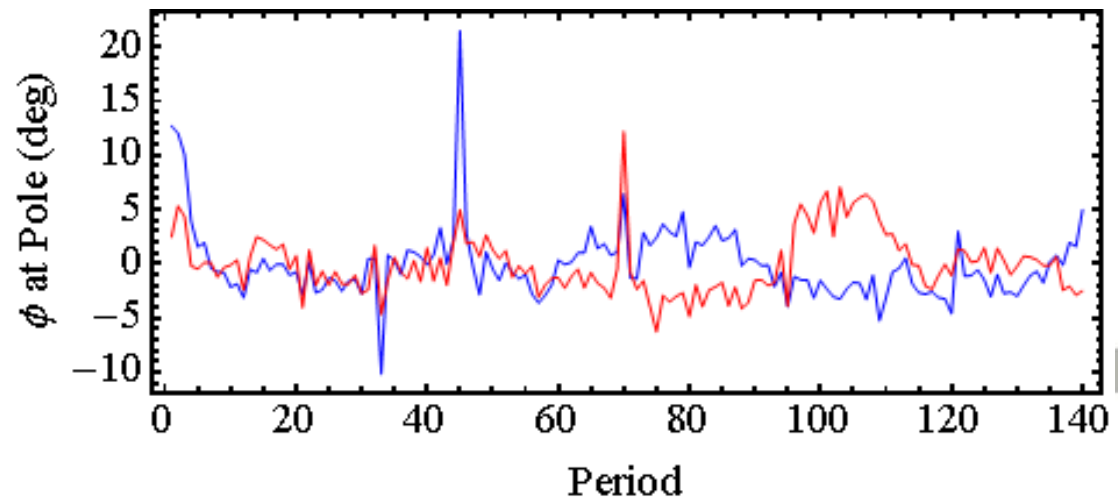
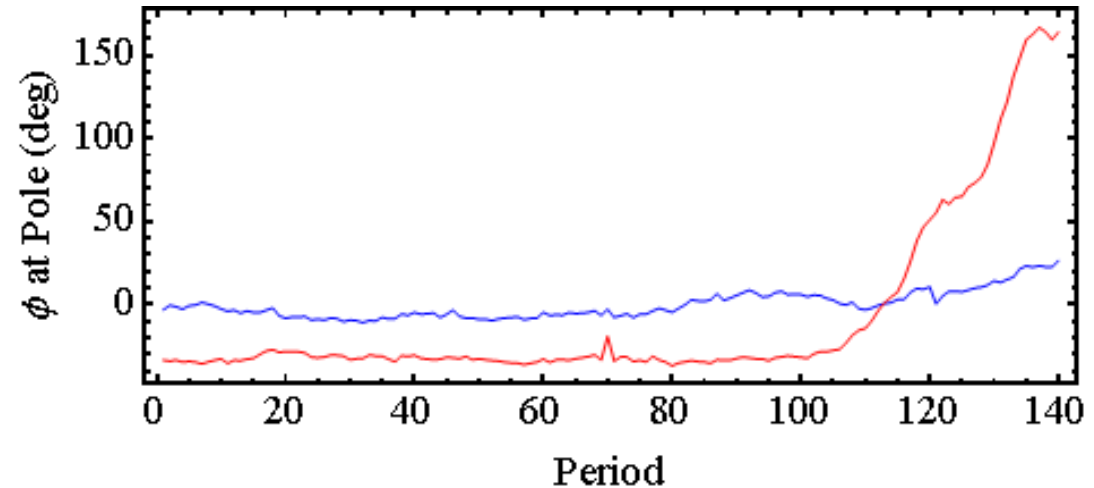
$$\sigma_{\phi X} = 8.3^{\circ}$$

$$\sigma_{\phi Y} = 53^{\circ}$$

- Magnet 2

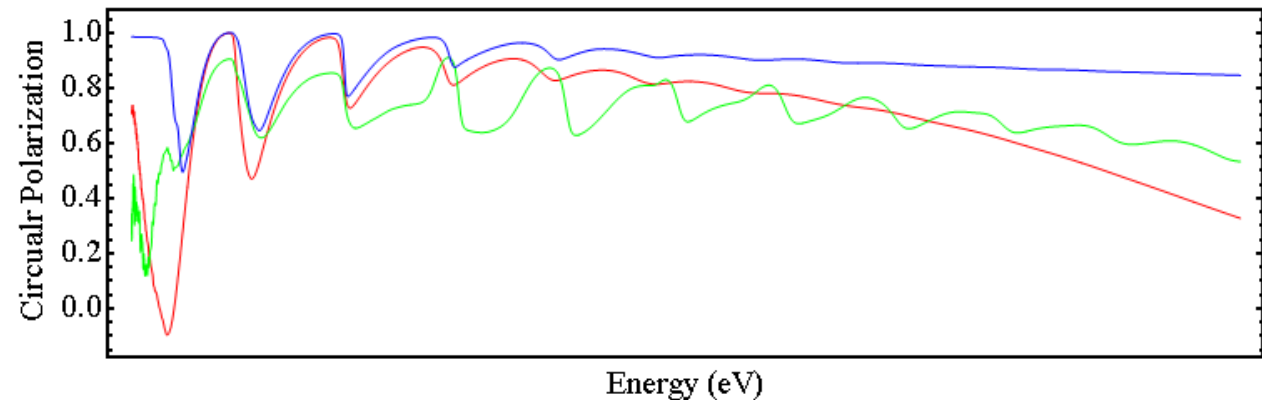
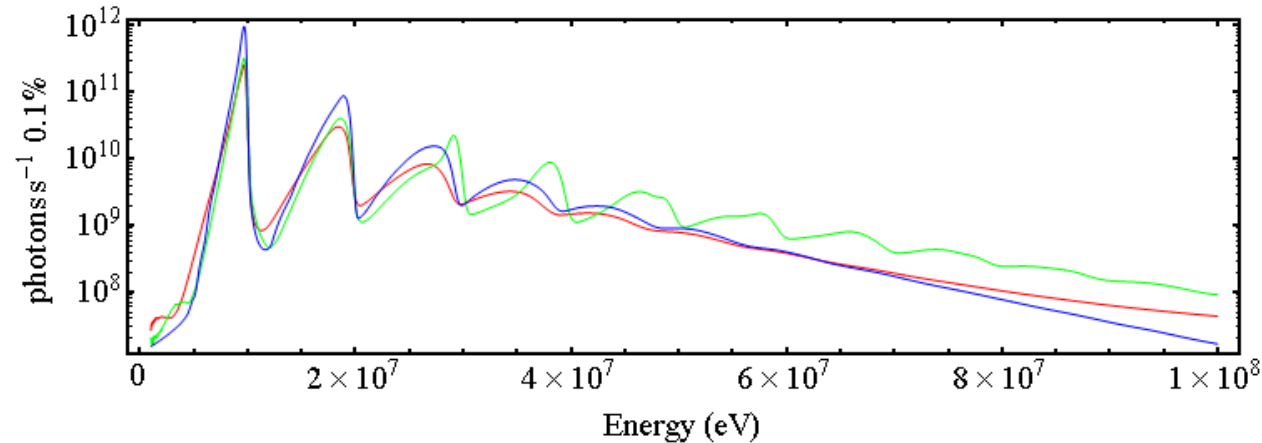
$$\sigma_{\phi X} = 3.4^{\circ}$$

$$\sigma_{\phi Y} = 2.8^{\circ}$$

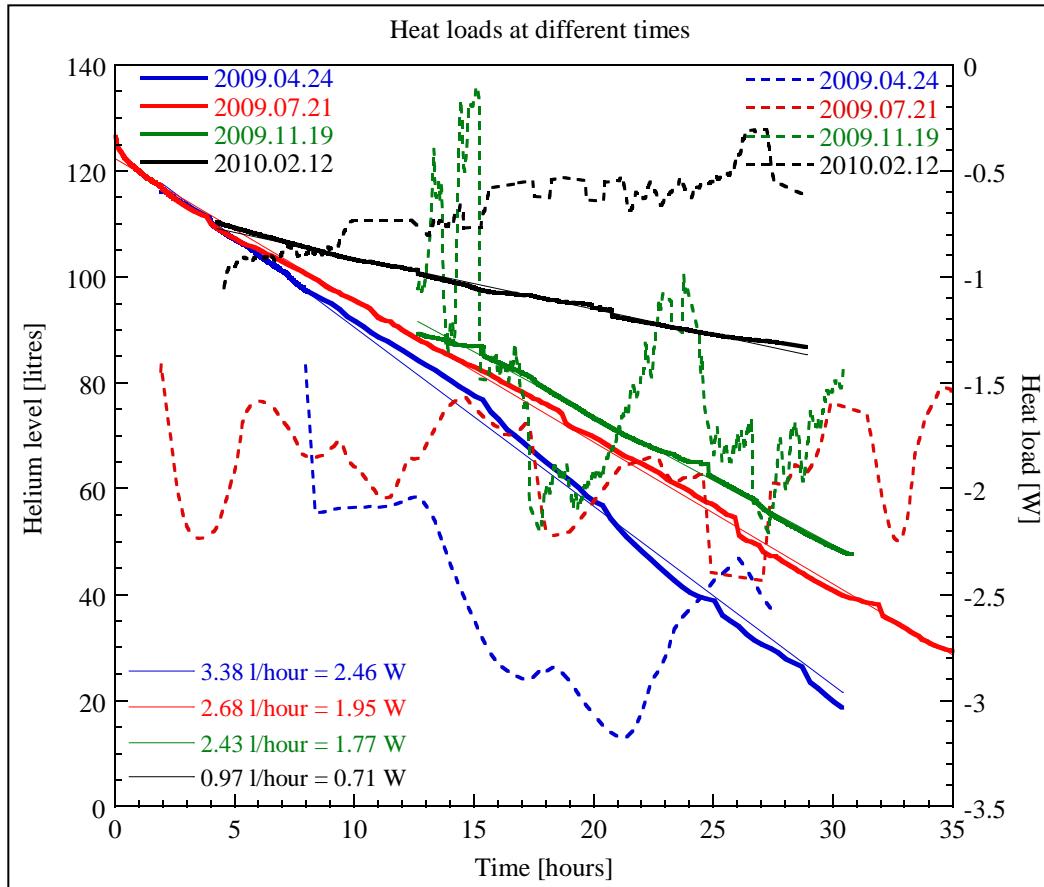


# Flux calculated with SPECTRA

- Flux into 1 $\mu$ rad square aperture, red M1, green M2, blue ideal
- Issue – there are more high energy photons than ideal case (although not more total power)
- Investigating this now with our own code and one written in C



# Module Heat Load Problem



- Heat load higher than anticipated
  - System is not recondensing
- Improvements being made slowly with time
  - Main issue is top plate not at **4K**





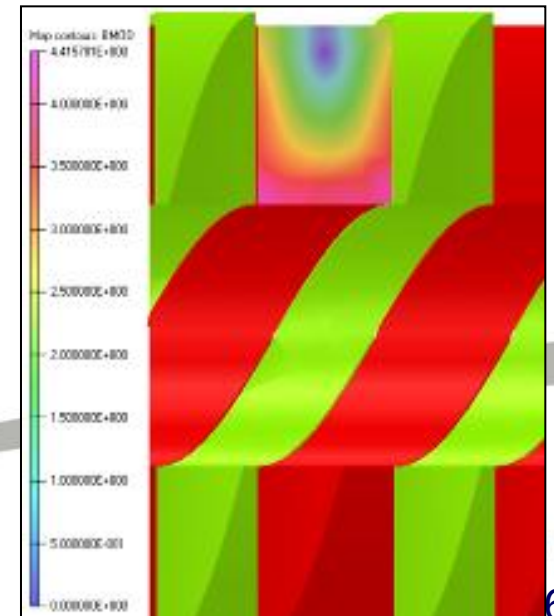
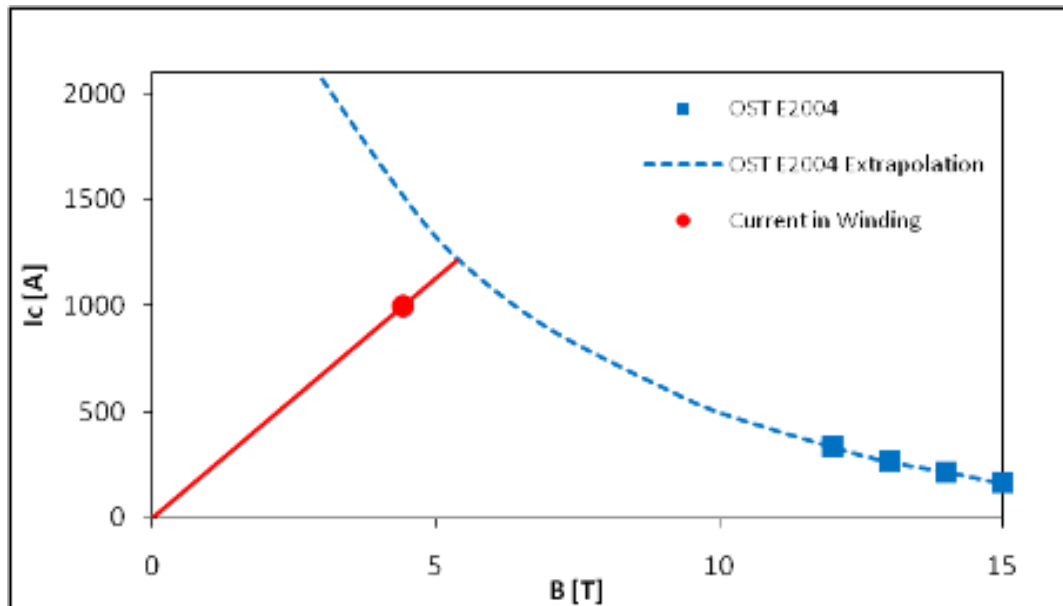
# Application of Nb<sub>3</sub>Sn

- To generate higher fields or to be able to reduce the period we need to use Nb<sub>3</sub>Sn
- Goal would be to reduce period to ~9mm
- **Concerns**
  - Packing factor reduced as insulation is thicker
  - Performance of wire at <5T
  - Insulation of former
  - Can no longer wind with ribbon
  - More difficult material to work with (heat treatment)
- Need Nb<sub>3</sub>Sn wire to have small diameter for similar filling factor
- Have purchased 1 km of Ø0.5 mm (Ø0.63 mm with glass braid) wire from OST.



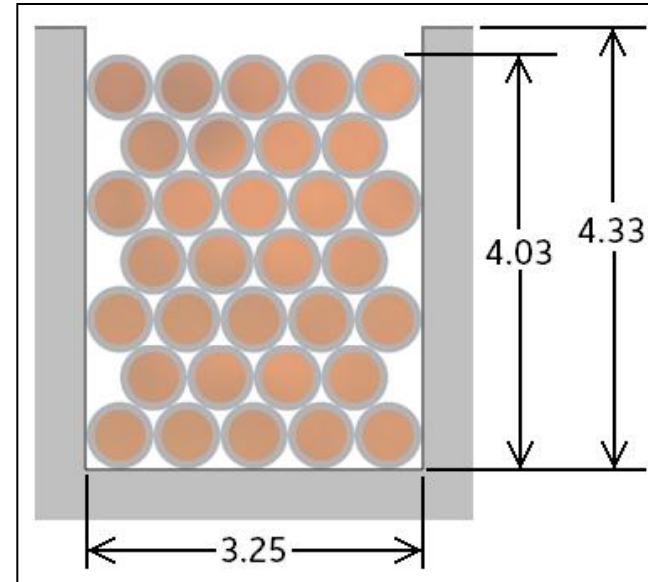
# FEA Modelling

- Winding ID:  $\text{O}6.35$  mm as before
- Field on axis: 1.54 T For 11.5mm period (cf 0.86T)
- Peak field in conductor: 4.4 T
- Operating at 82% of  $I_c$
- Wire performance to be measured at  $\sim 5$ T by KIT

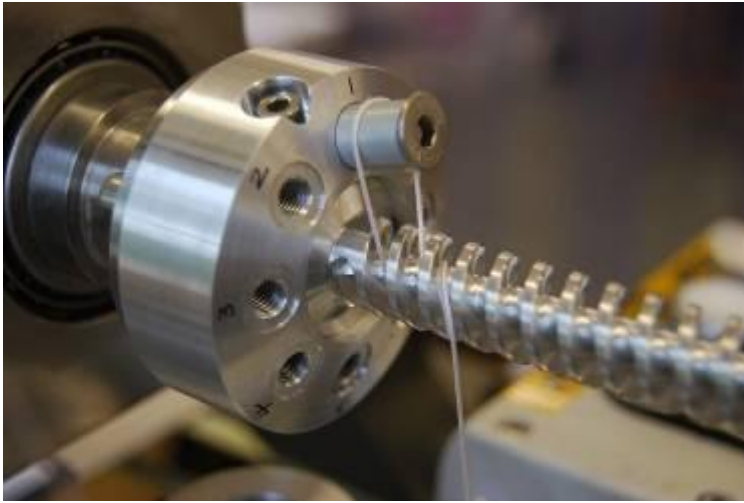


# Trial Winding

- Need to do a trial winding to confirm groove dimensions
- Aluminium Former has been made with the dimensions shown
- Will be 32 wires in winding
- 11.5 mm period
- Will be wound, potted and sectioned to check groove width etc



# Trial Winding



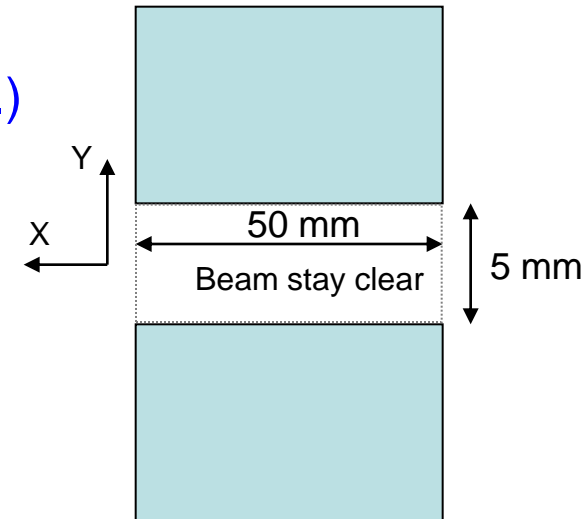
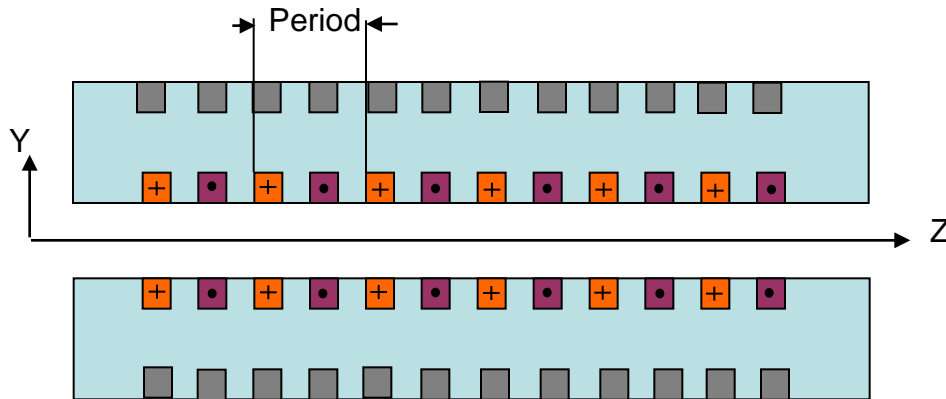
# Planar SCU for Light Sources

- Successful helical undulator project helped secure funding for planar studies
- Same team of people
- Diamond has recently joined project
- It is anticipated that the first planar SCU will be installed into Diamond (~2012)



# Undulator Specifications

|                          |                               |
|--------------------------|-------------------------------|
| Magnetic length:         | 2 m                           |
| Period :                 | 15 mm                         |
| Field on axis:           | 1.4 T                         |
| K                        | 2.0                           |
| Beam stay clear:         | 5 mm (Vert.) x 50 mm (Horiz.) |
| rms phase error:         | < 3 degrees                   |
| Trajectory straightness: | +/- 0.5 micron                |



# Design Features

- Cold bore magnet with **5mm** aperture vacuum vessel at **~12K**
- Magnet gap **7mm** to allow vacuum gap between vessel and magnet poles
- Magnet to operate at **~1.8K** in order to reach desired field level on axis
- Closed cycle pumped cryo system to achieve 1.8K

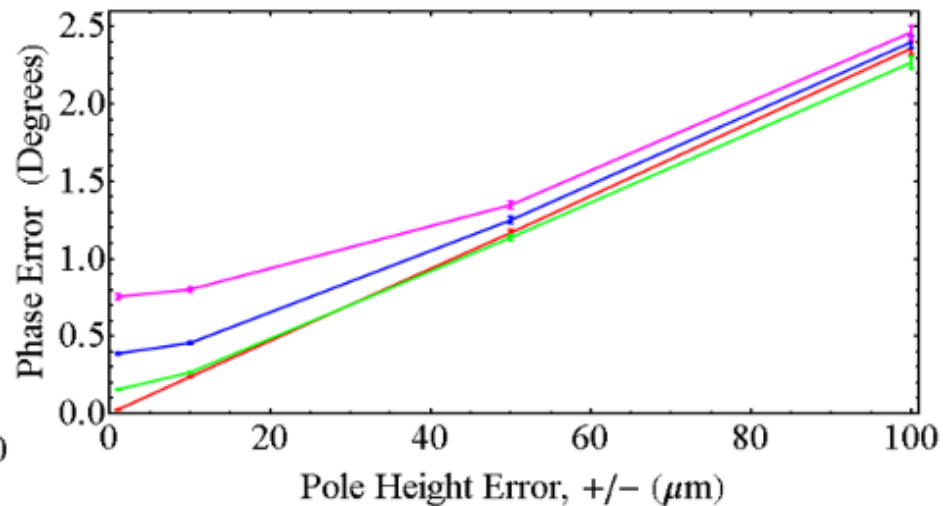
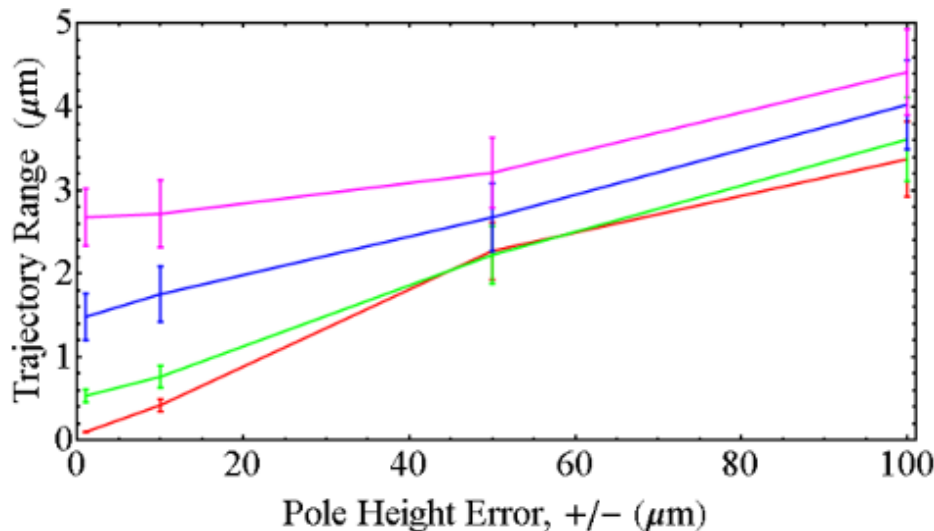






# Radia Modelling

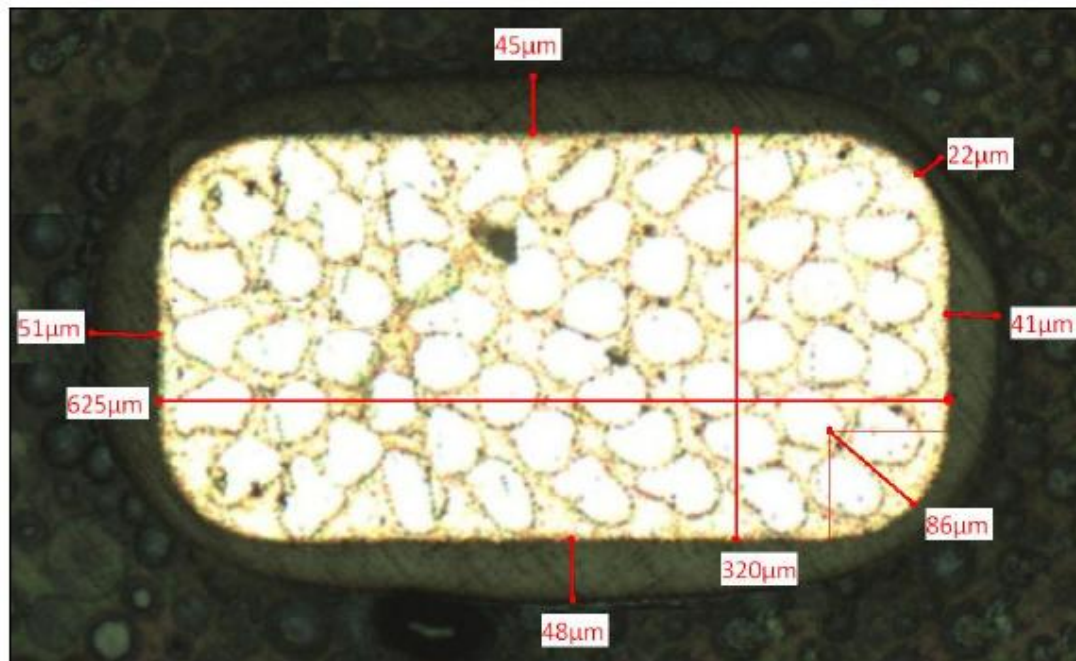
- Effect of errors in pole dimensions suggest that with  $\pm 10 \mu\text{m}$  in height and  $\pm 50 \mu\text{m}$  in length the specification can be met



Effect of pole height error for a pole length error of  $\pm 1 \mu\text{m}$  (red),  $\pm 10 \mu\text{m}$  (green),  $\pm 50 \mu\text{m}$  (blue) and  $\pm 100 \mu\text{m}$  (magenta)  
Error bars define 99% confidence levels

# SC Wire

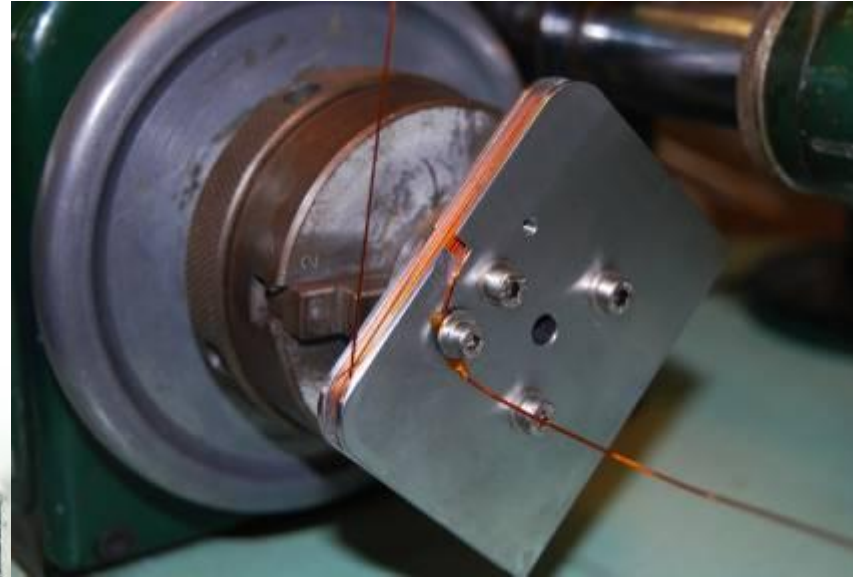
- NbTi procured from Supercon
- Cu:SC of 0.9:1.0
- 0.5mm diameter round wire has been rolled to rectangular to improve packing factor



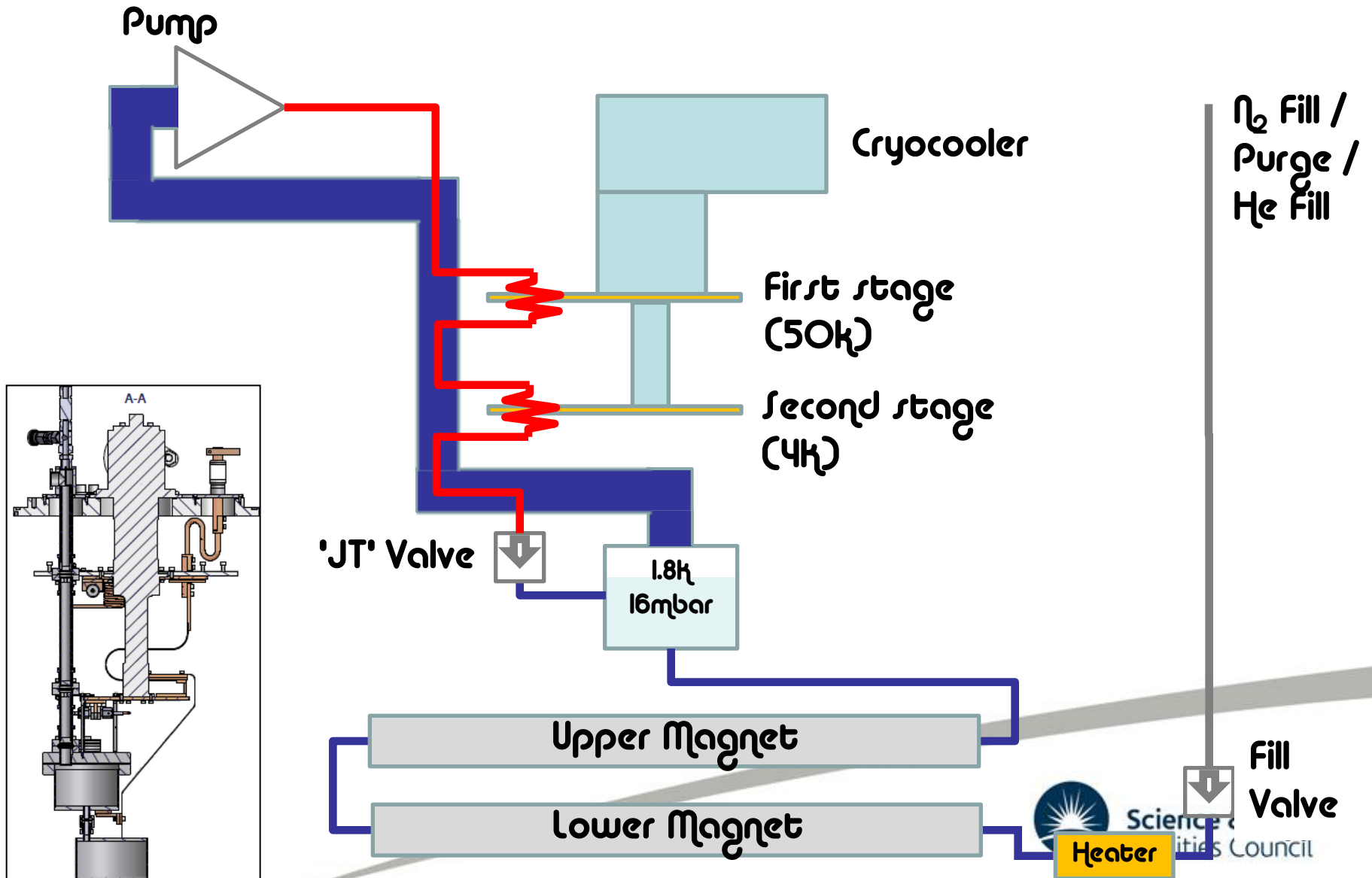
# Winding and Former Trials

Initial winding trials have been done with a single coil former and rectangular section (0.635mm x 0.305mm) insulated Cu wire.

Objective was to devise a winding/potting procedure which would position/align the wires to within 10 microns in y.

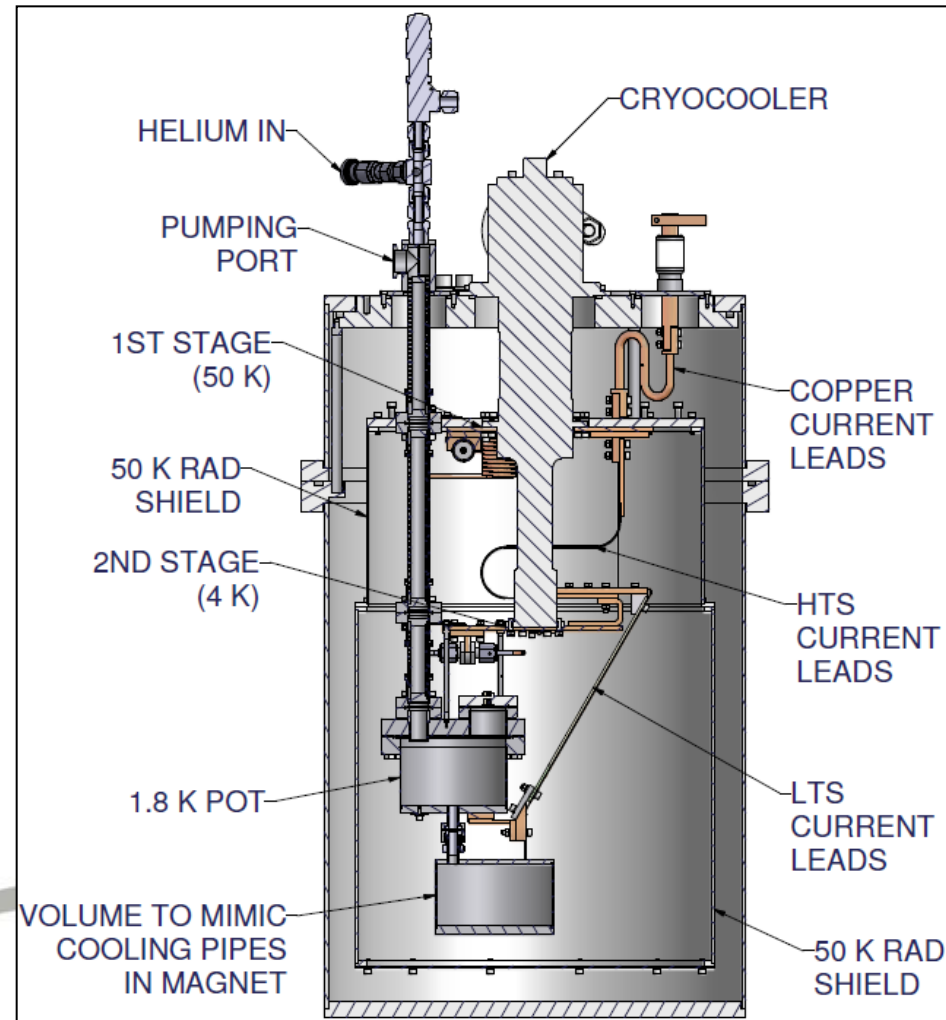
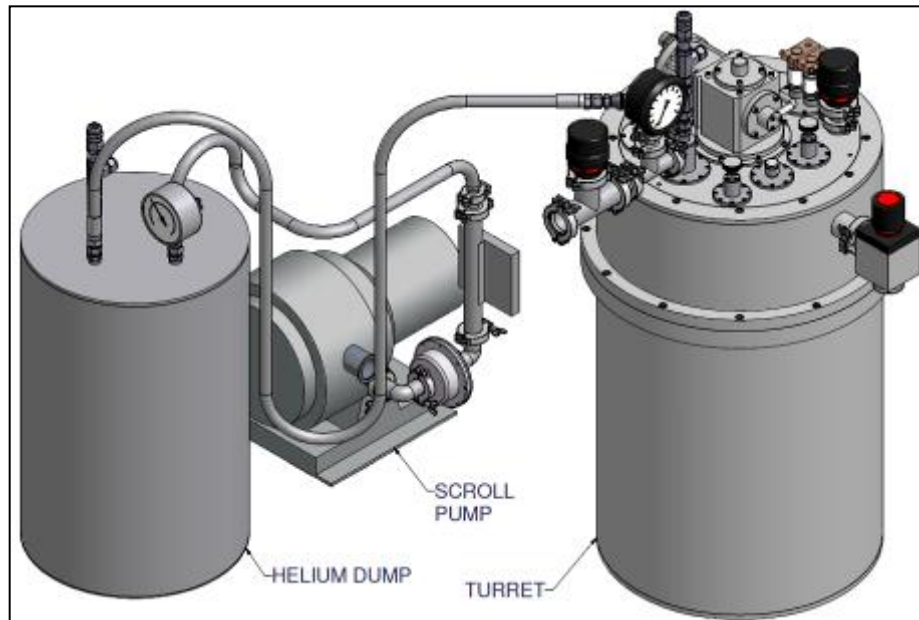


# Conceptual Layout of Turret

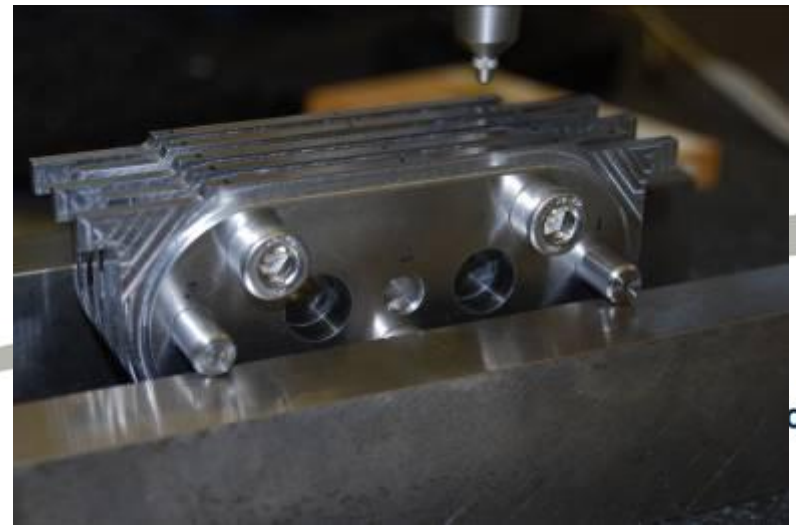
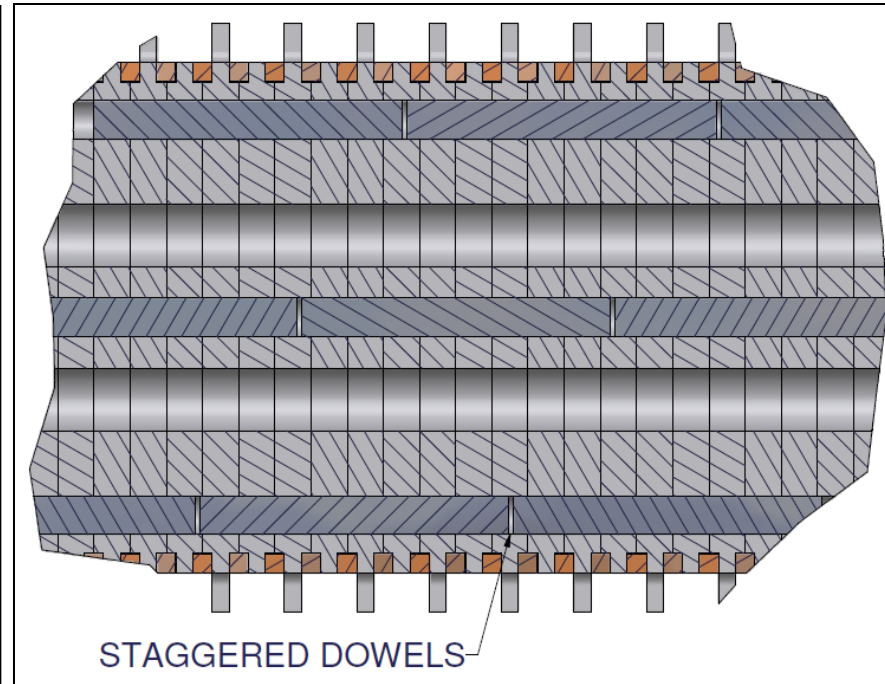
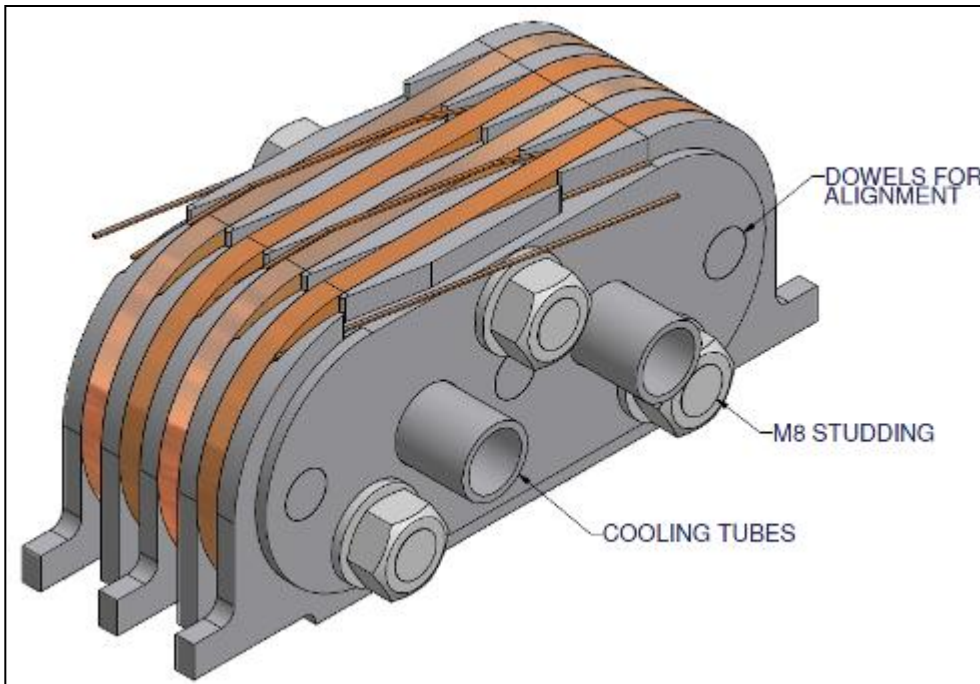


# Cryogenic Turret

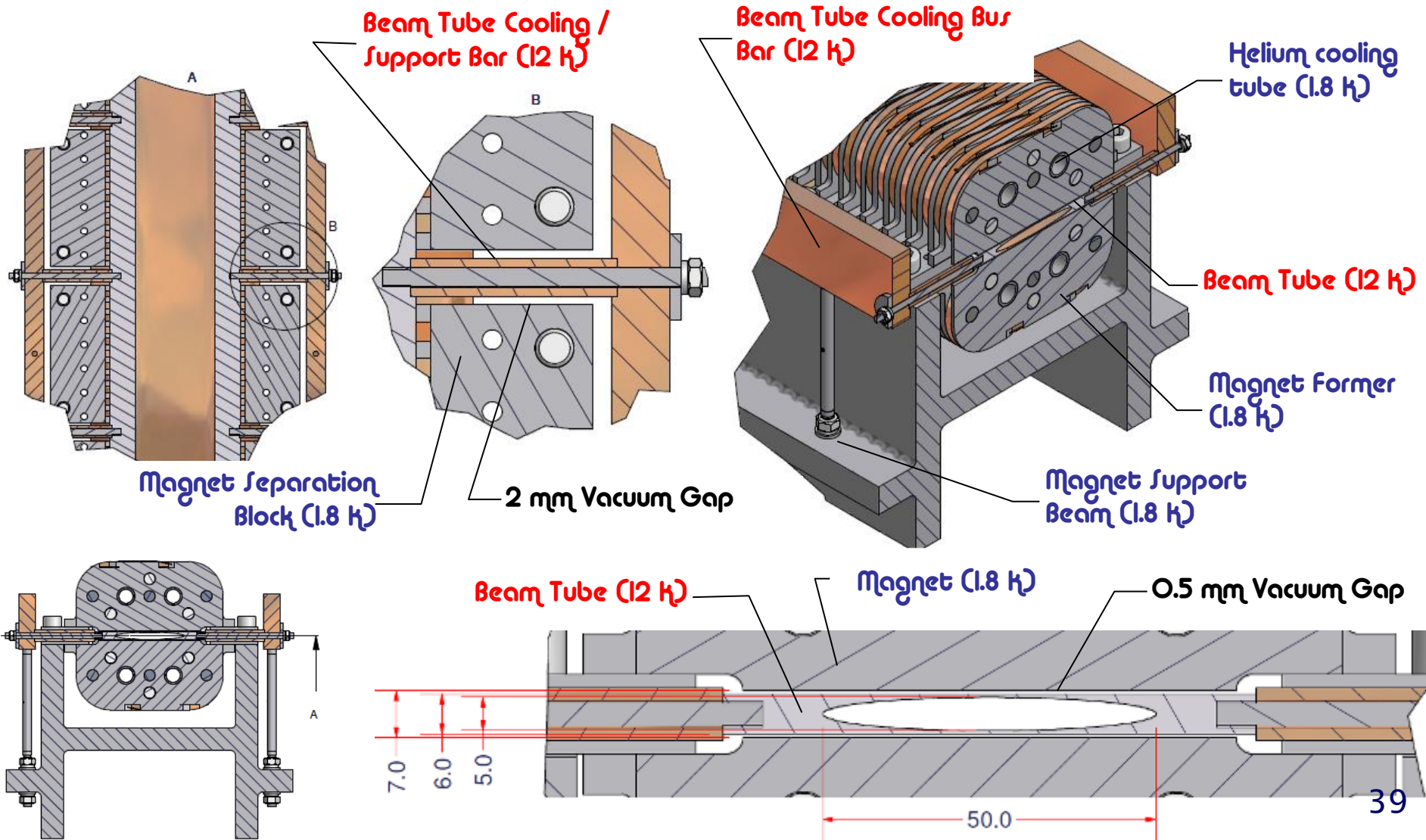
- 200 mW of cooling power at 1.8 K with only 0.68 W load on Cryocooler 2nd stage
- Most parts now delivered
- Will be tested in isolation prior to full magnet construction
- Contains dummy load with heater



# Undulator Magnet



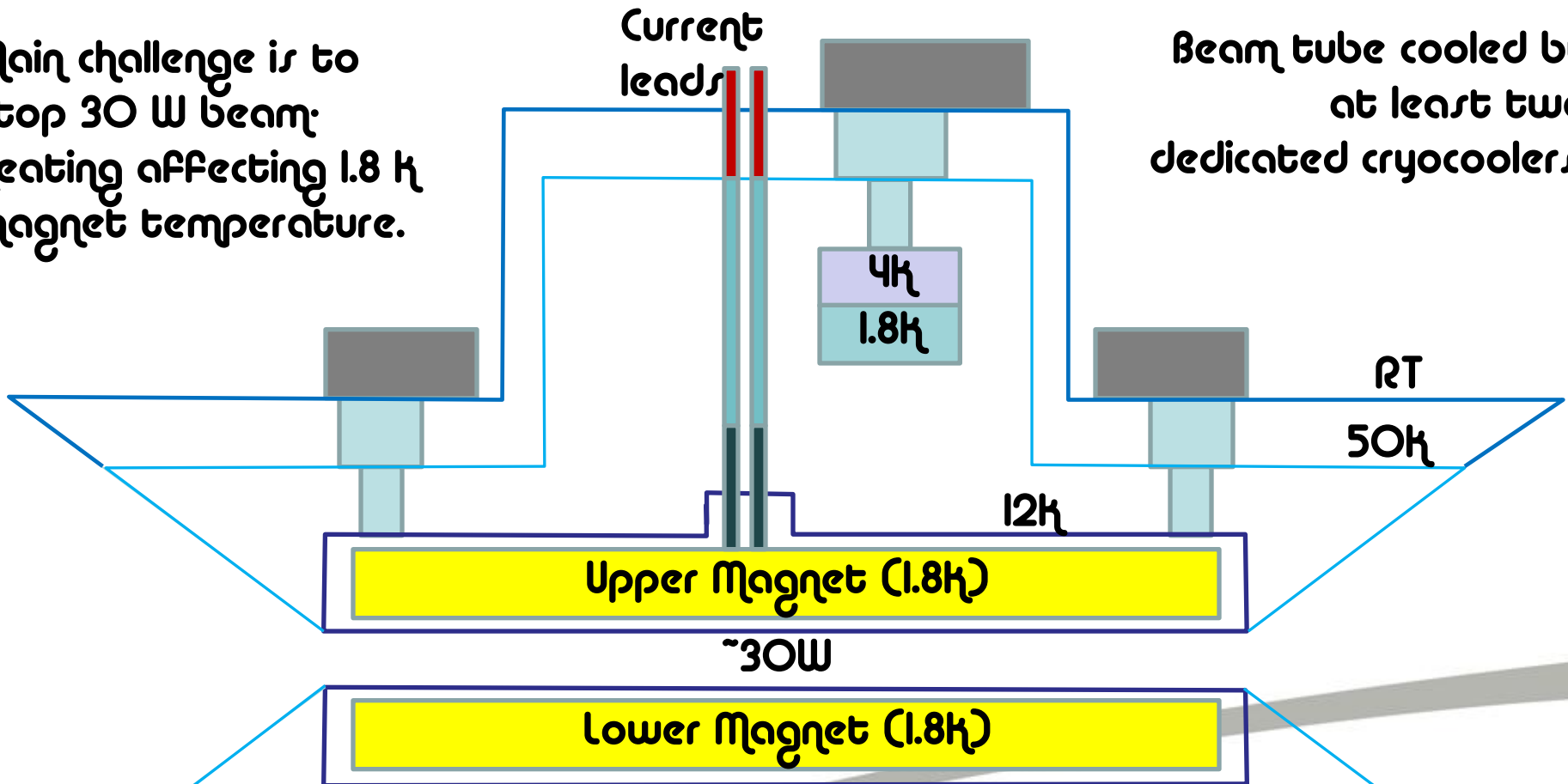
# Undulator Assembly



# Conceptual Layout of Cryostat

Main challenge is to stop 30 W beam heating affecting 1.8 K magnet temperature.

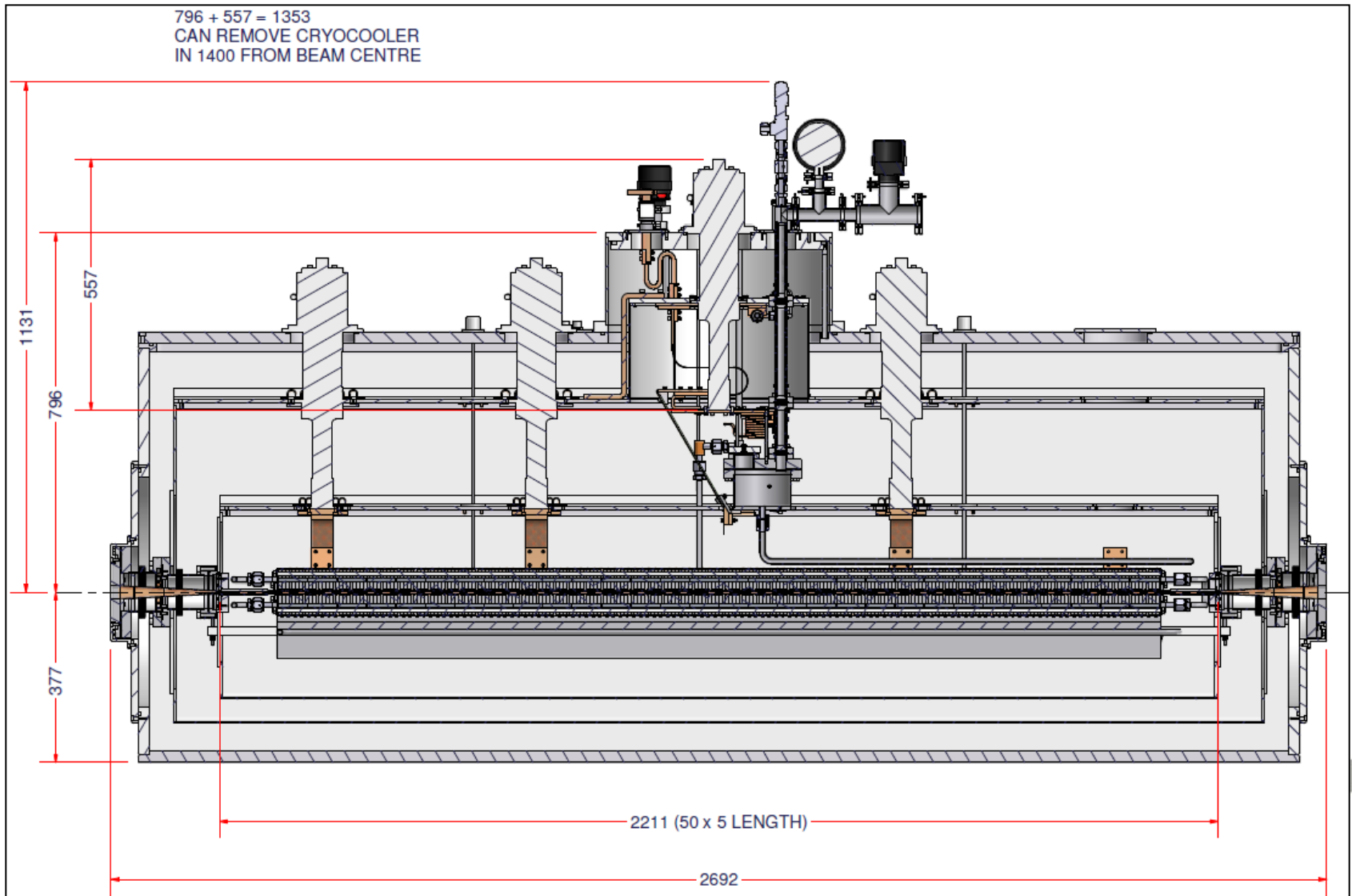
Beam tube cooled by at least two dedicated cryocoolers.





# Complete Undulator

$796 + 557 = 1353$   
CAN REMOVE CRYOCOOLER  
IN 1400 FROM BEAM CENTRE



# Planar Future Steps

- Assemble the turret test rig and confirm the cooling powers expected are achieved
- Construct a short magnet array to confirm tolerances are achieved
- Construct and vertically test full length magnet
- Assemble and test complete undulator
- Install into Diamond and confirm cryo and magnetic performance



# Resistive Wakefields

- Resistive Wakefields rely on computing the interaction of an external field with the “electrical properties” of the environment
  - External field – electron bunch
  - Environment – Conductivity & shape of vessel
- Different conductivity models are used:
  - DC Conductivity
  - AC Conductivity
    - frequency dependant
  - Anomalous Skin Effect
    - The skin depth is small compared to the mean distance between collisions
  - Extreme Anomalous Skin Effect
    - Behaviour at very low temperatures (<4K)

$$\sigma_{AC} = \frac{\sigma_0}{1 - i\omega\tau}$$

Mean time between collisions for an electron



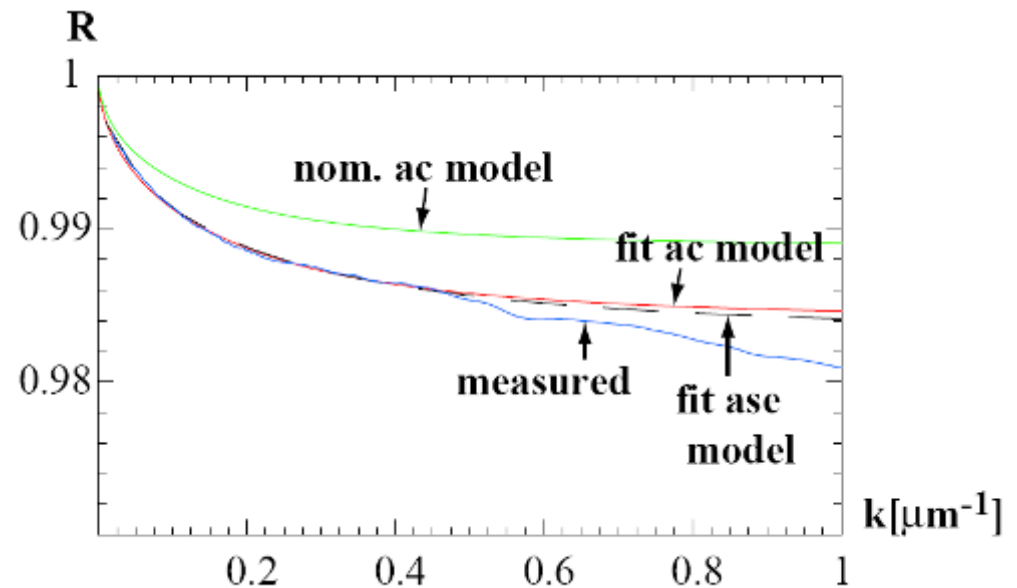
# Simulations

- The resistive wakefield is often the limiting factor for how narrow the magnet aperture can be
- Especially important for predicting heat load on cold bore SCUs
- Simulations can only be as accurate as the material properties entered into the codes
- Material properties are not well known, especially at 4K
- Effect of coatings (eg copper or NEG) not clear



# Measurements

- To accurately model the conductivity we need to accurately measure it
- Optical properties of metals:
  - From a measurement of the reflectivity of a metallic surface the conductivity can be inferred
  - **Difficult to measure accurately**



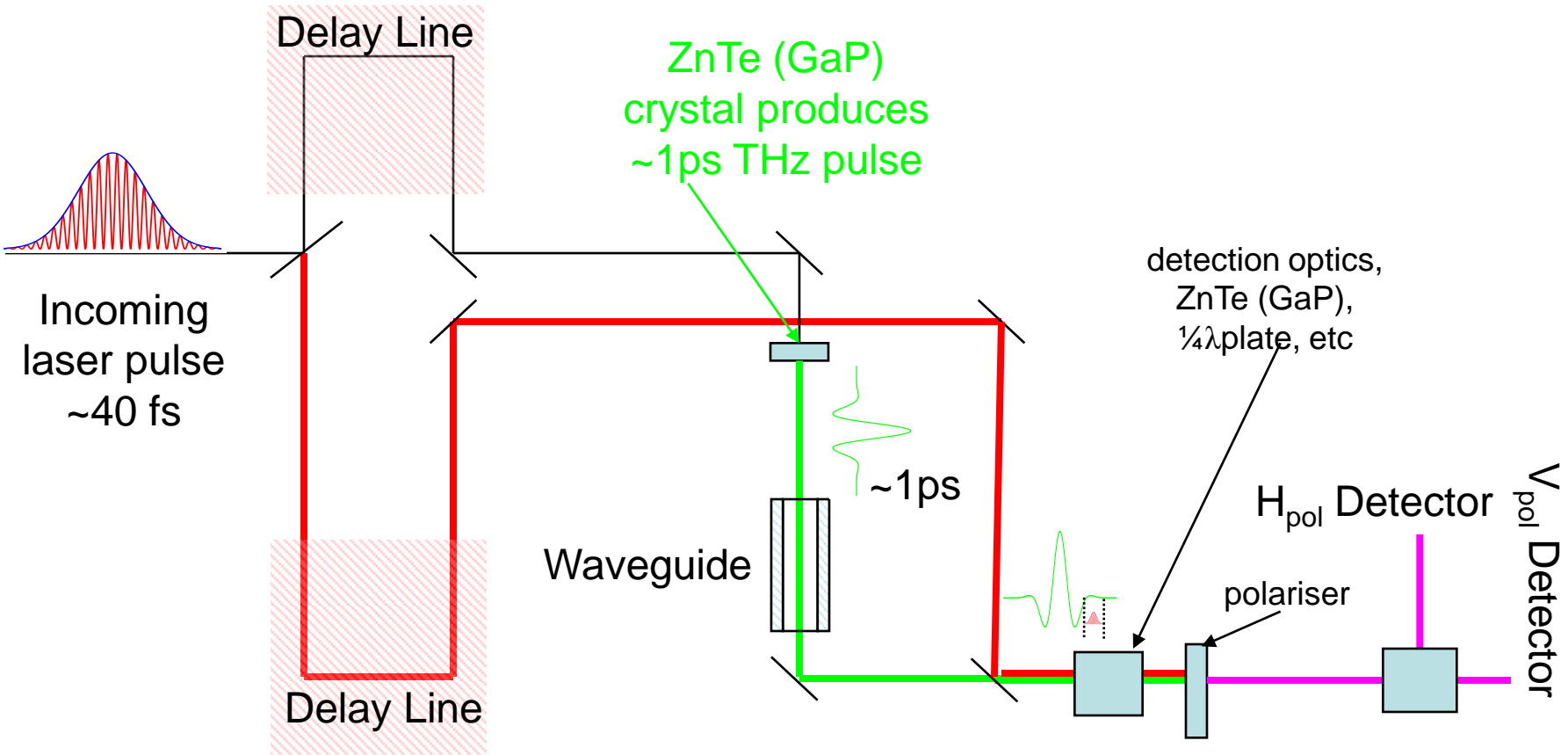
(Bane, Stupakov & Tu)

# Measurements

- Measure the attenuation and dispersion of EM THz signal passing through the vessel – which acts as a waveguide.
  - Signal to noise ratio much higher
  - Can measure the actual beam pipe that will be used
  - Waveguide theory enables us to calculate the mode structure of the THz and the mode propagation
  - Cylindrical vessels, rectangular vessels, elliptical vessels, etc
  - Compare theory to experiment
  - Warm or cold vessels possible



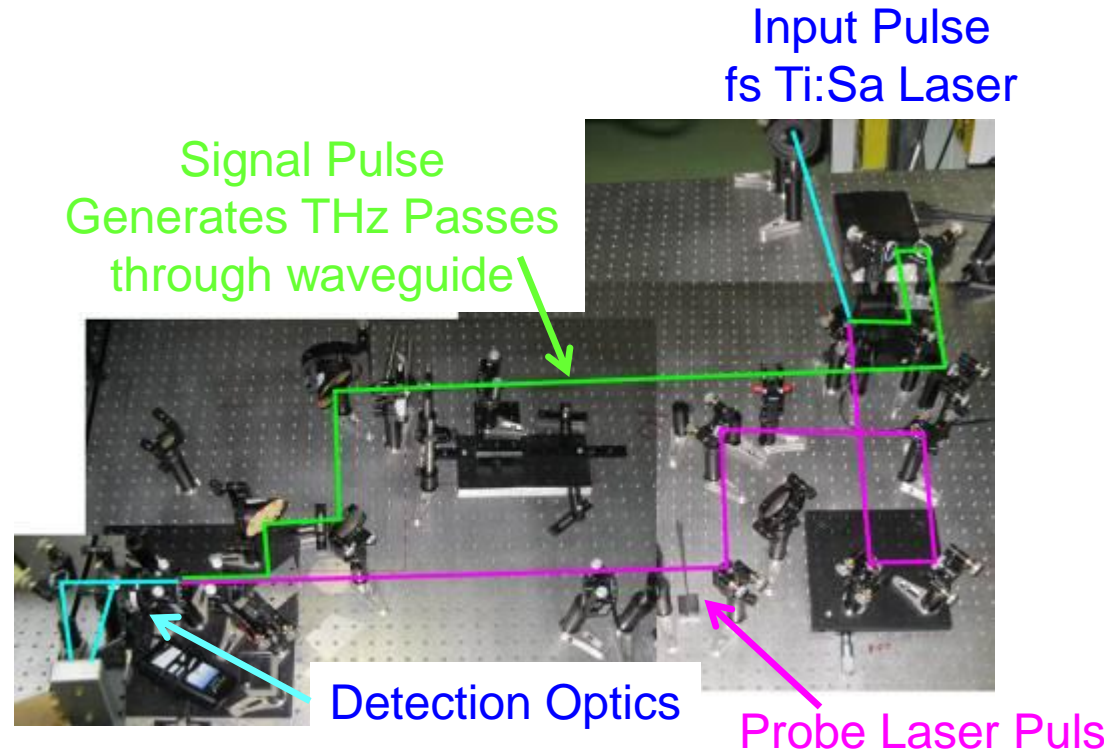
# Experimental set-up



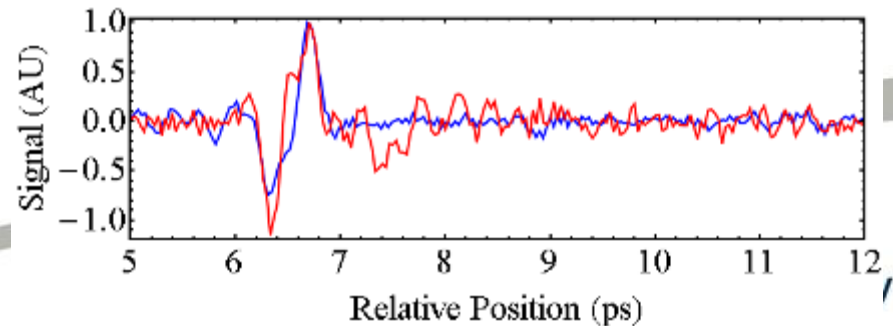
- sub-picosecond time-resolved measurement of the attenuation and dispersion of a THz pulse (generated by optical rectification) through a waveguide

# Initial Results

- First stage: get experiment working with simple rectangular and circular waveguides at room temperature
- First results encouraging
- Measure difference signal between two different length waveguides



Measured  
Theory





# Summary

- SCU Helical constructed from NbTi and full spec achieved (0.86T @ 11.5mm)
- Nb<sub>3</sub>Sn short prototypes will be constructed soon (1.5T @ 11.5mm?)
- SCU Planar design virually complete (NbTi)
  - 1.4T @ 15mm, 1.8K magnet with 5mm beam aperture
- Winding trials underway
- Turret system procured and will be assembled and performance confirmed soon
- Experiment technique developed to measure directly the electrical properties of warm or cold vacuum vessels
  - Initial results promising

